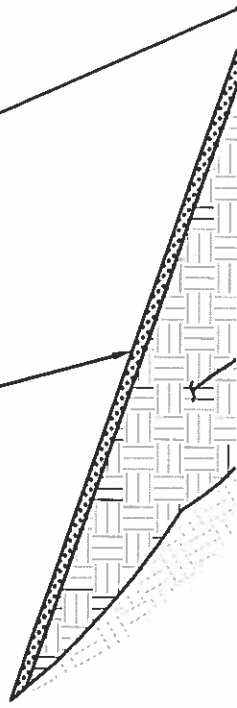
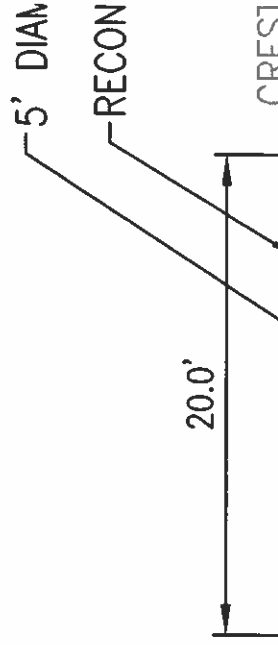
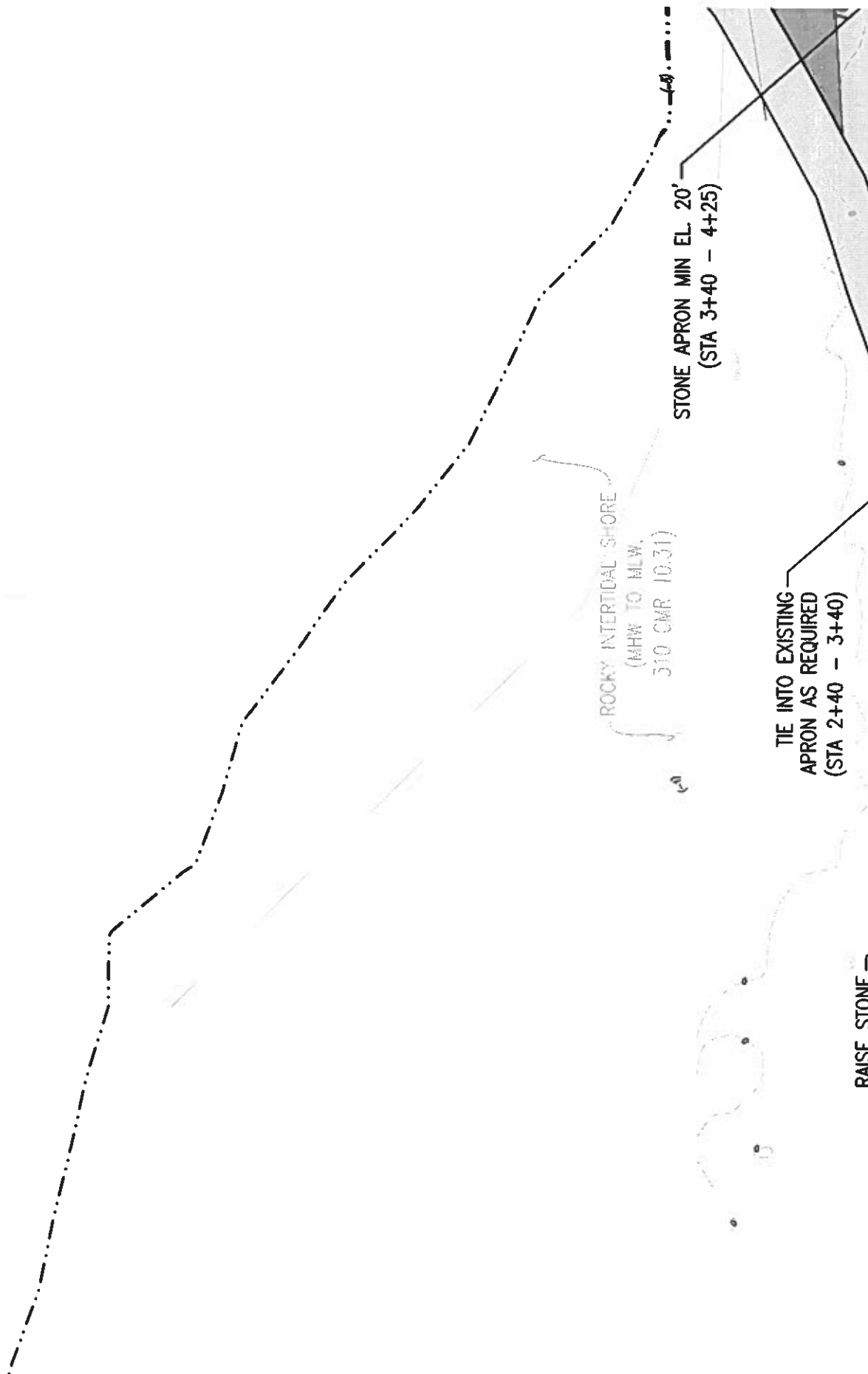


CONCRETE
DRAINAGE SWALE
LOAM AND SEED



CONCRETE SWALE TO BE CAST
INTO APRON AS REQUIRED





STONE APRON MIN EL. 20'
(STA 3+40 - 4+25)

ROCKY INTERTIDAL SHORE
(MHW TO MLW,
510 CMR 10.31)

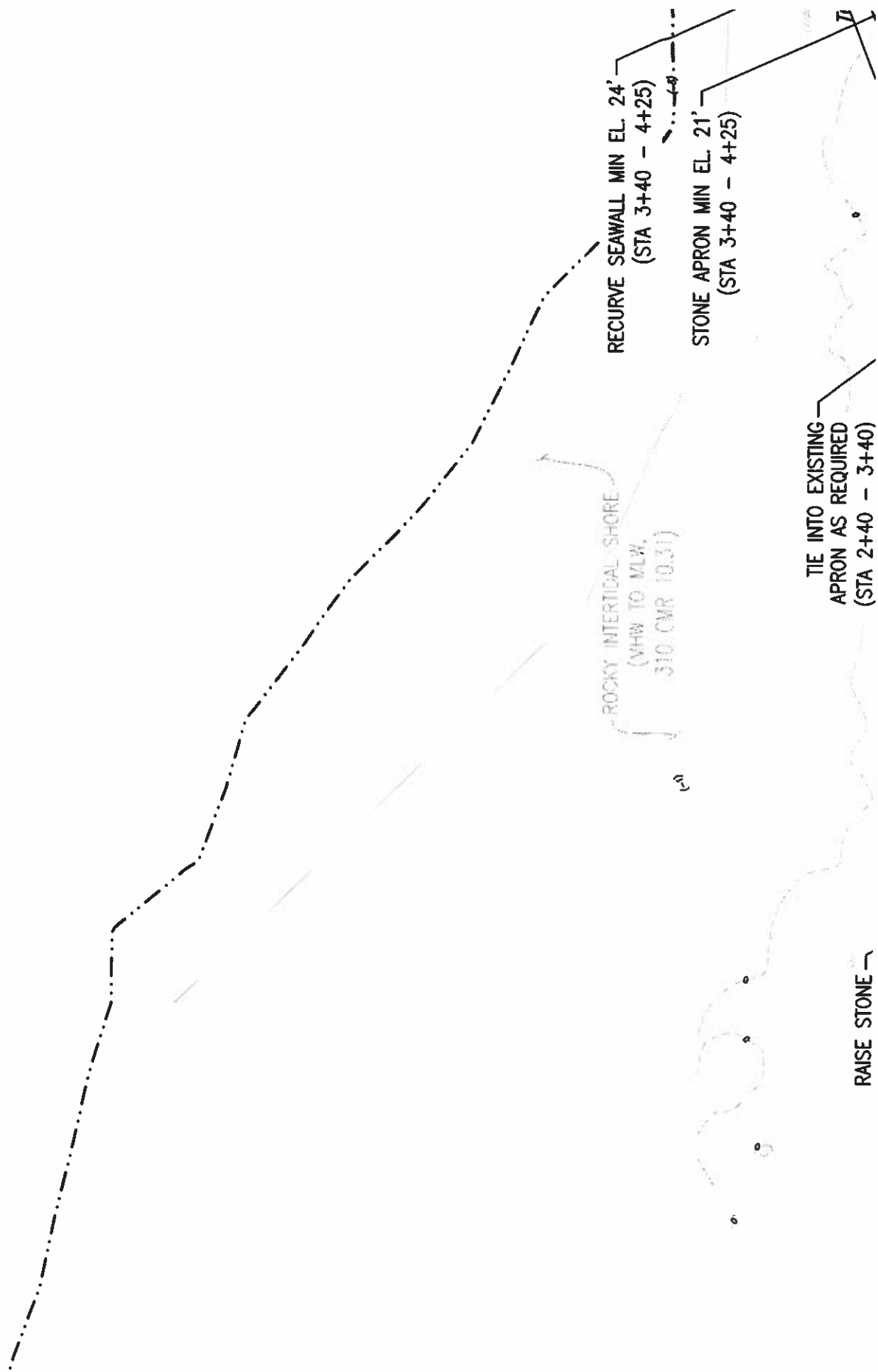
TIE INTO EXISTING
APRON AS REQUIRED
(STA 2+40 - 3+40)

RAISE STONE

RECONSTRUCT F
BERM CREST AS

CONCRETE
DRAINAGE
SWAIF

LOAM AND



CAST-IN-PLACE CONCRETE
SWALE AND APRON

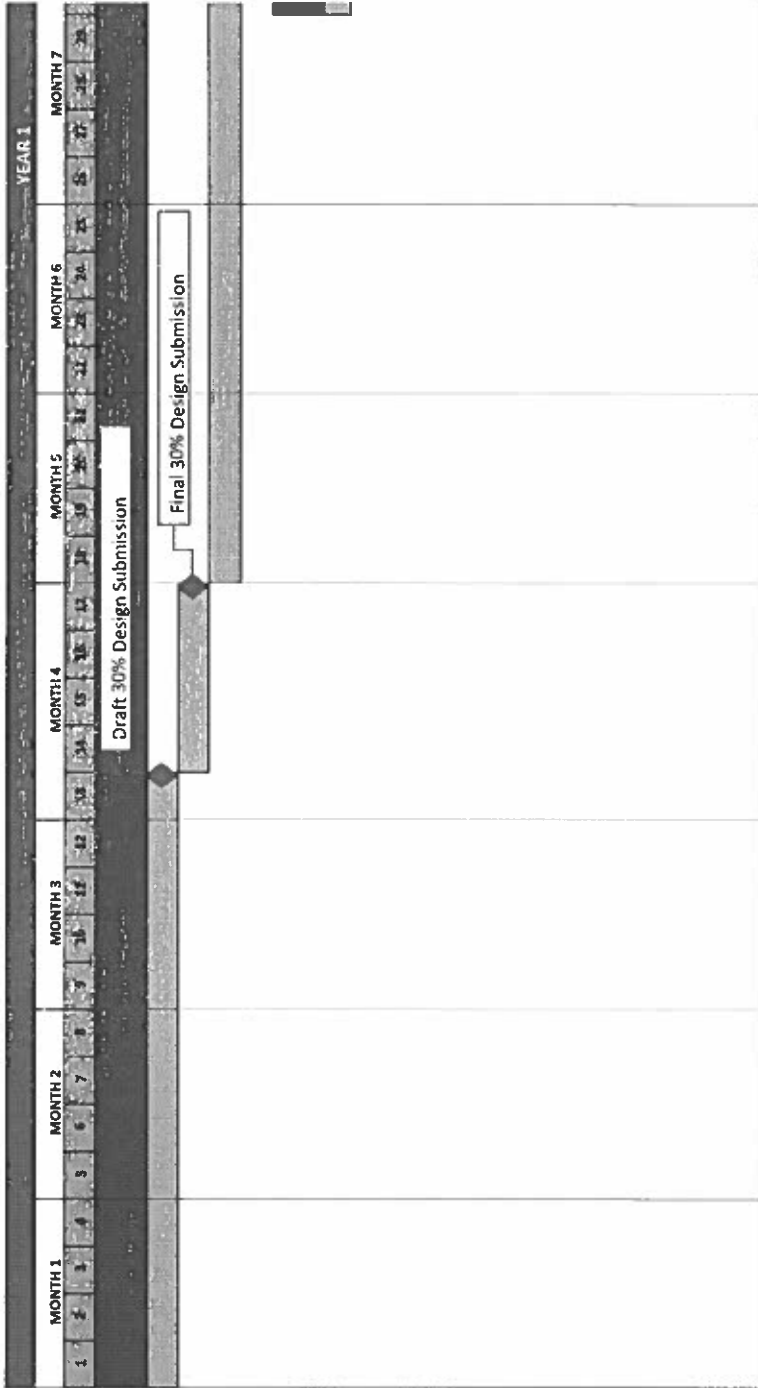
35'



ATTACHMENT B
Estimated Project Timeline

ESTIMATED PROJECT TIMELINE

TASK	START	END
1 - DESIGN DEVELOPMENT	MONTH 1 - MONTH 10	
Draft 30% Design	14 weeks	
Review Period & Final 30% Design	4 weeks	
Draft 75% Design	20 weeks	
Review Period & Final 75% Design	4 weeks	
2 - PERMITTING	MONTH 7 - MONTH 54	
MEPA ENF	21 Weeks	
ConCom Notice of Intent	10 weeks	
USACE Individual Permit *	65 weeks	
401 WQC **	60 weeks	
Chapter 91 License **	68 weeks	
MESA Review Filing	4 weeks	
Closeout Requirements	4 weeks	
3 - CONTRACT DOCUMENTS	MONTH 31 - MONTH 35	
100% Design	16 weeks	
Bid Documents	5 weeks	
4 - CONSTRUCTION PHASE SERVICES	MONTH 36 - MONTH 54	
Construction Phase	78 weeks (assumed)	



Notes:

1. The schedule has been developed to depict the anticipated progression of work throughout the duration of the Project, assuming permit applications are Submitted as shown on the schedule.
2. The milestones and timelines reflect our best reasonable judgement including submissions, review periods, and minimal float time to meet the overall project deadlines. The actual schedule may be accelerated.
3. Construction Phase Services task does not consider time of year (TOY) restrictions that permitting agencies may require for in-water construction work. The construction schedule may be extended depending on TOY restrictions.

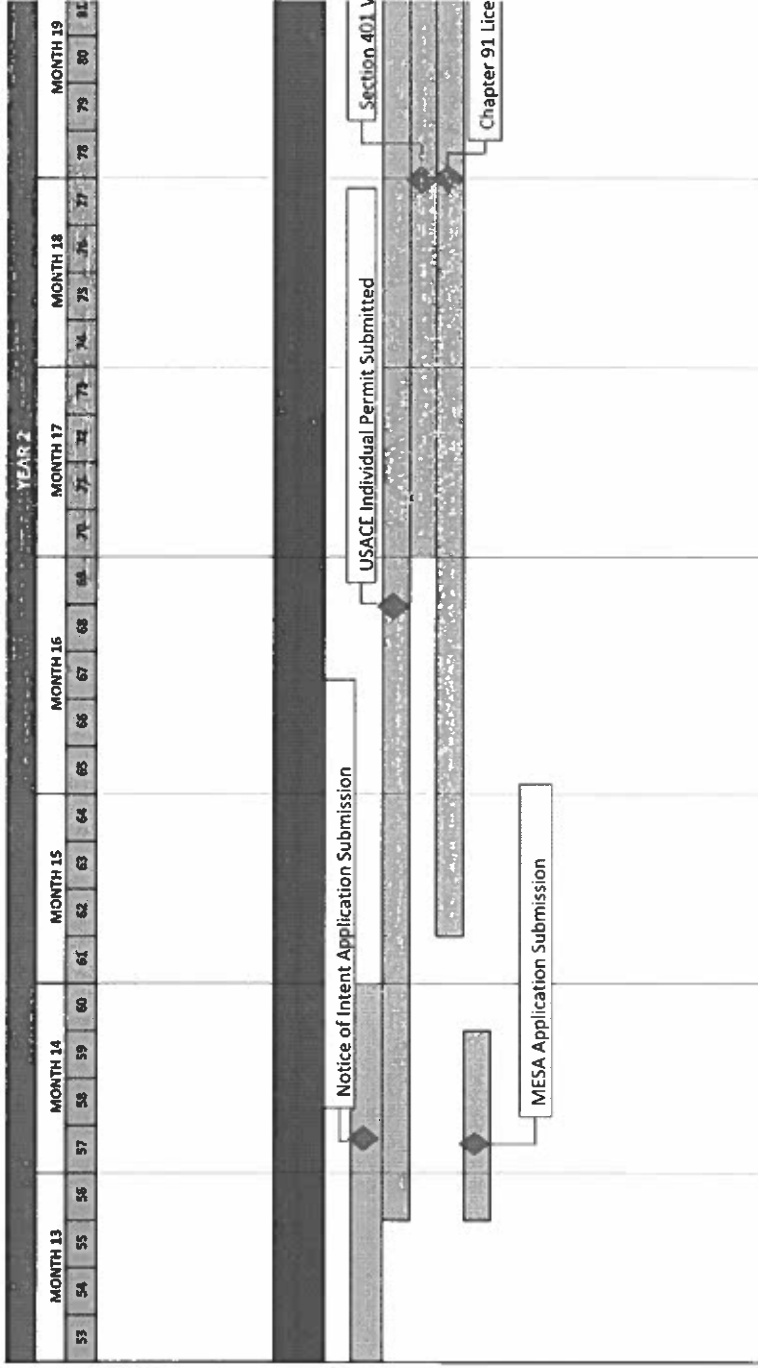
* USACE regulations indicate that individual Permit decisions are typically made within two to three months. However, based on recent experience obtaining USACE permits, it is possible that the review time may be extended.

** MassDEP Waterways regulations do not indicate anticipated permit review timelines, but the schedules shown are based on recent experience obtaining Chapter 91 Licenses and Section 401 Water Quality Certifications.

- ◆ = Milestone
- ▬ = Schedule Breakline

ESTIMATED PROJECT TIMELINE

TASK	START	END
1 - DESIGN DEVELOPMENT	MONTH 1	MONTH 10
Draft 30% Design	14 weeks	
Review Period & Final 30% Design	4 weeks	
Draft 75% Design	20 weeks	
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USACE Individual Permit *	65 weeks	
401 WQC **	60 weeks	
Chapter 91 License **	68 weeks	
MESA Review Filing	4 weeks	
Closeout Requirements	4 weeks	
3 - CONTRACT DOCUMENTS	MONTH 31	MONTH 35
100% Design	16 weeks	
Bid Documents	5 weeks	
4 - CONSTRUCTION PHASE SERVICES	MONTH 36	MONTH 54
Construction Phase	78 weeks (assumed)	



TASK	START	END
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Draft 75% Design	20 weeks	
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2 - PERMITTING		
	MONTH 7 - MONTH 54	
MEPA ENF	21 Weeks	
ConCom Notice of Intent	10 weeks	
USACE Individual Permit *	65 weeks	
401 WQC **	60 weeks	
Chapter 91 License **	68 weeks	
MESA Review Filing	4 weeks	
Closeout Requirements	4 weeks	
3 - CONTRACT DOCUMENTS		
	MONTH 31 - MONTH 35	
100% Design	16 weeks	
Bid Documents	5 weeks	
4 - CONSTRUCTION PHASE SERVICES		
Construction Phase	78 weeks (assumed)	

YEAR 3																											
MONTH 31			MONTH 32			MONTH 33			MONTH 34			MONTH 35			MONTH 36												
130	131	132	133	134	135	136	137	138	139	140	141	142	143	144	145	146	147	148	149	150	151	152	153	154	155	156	157
[Blank grid area for task scheduling]																											

ATTACHMENT C
Conceptual Cost Estimate



Point Allerton Coastal Engineering Shore Protection - Design Alternatives

Conceptual Cost Estimate

Alternative 1 - Retention Reconstruction

Item	Quantity	Unit	Unit Price	Total Cost*	Notes	Source
Site Prep/Remove Control	1	LS	\$60,000	\$60,000	Fencing barriers, hubbly/hull socks, turbidity curtain	Recent project costs
Demolition and Removal	700	CF	\$175	\$122,500	Demolish existing revetment apron, and seawall as required	Recent project costs
Remove and Re-set Slope Revetment	1000	CF	\$175	\$175,000	Demolish existing stones to accommodate improvements, reinstallation	Recent project costs
Groutstone Fabric	6000	SF	\$11	\$66,000	Remove and install geotextile fabric	MS&D Weighted Bid Prices Item No. 698.1 and recent project costs (obtained 7/1/2024)
Furnish and Install Bedding and Crushed Stone	6900	TON	\$10	\$69,000	0.75 inch crushed stone bedding	MS&D Weighted Bid Prices Item No. 156.8 and recent project costs (obtained 7/1/2024)
Furnish and Install Core Stone	103500	TON	\$130	\$13,455,000	50 lb armor revetment stones with delivery	MS&D Weighted Bid Prices Item No. 156.8 and recent project costs (obtained 7/1/2024)
Furnish and Install Filter Stone	73000	TON	\$150	\$10,950,000	0.75 inch armor stone with delivery (includes slope protection / toe slope)	MS&D Weighted Bid Prices Item No. 156.8 and recent project costs (obtained 7/1/2024)
Furnish and Install Armor Stones	56000	TON	\$300	\$16,800,000	8-12 ton armor stone with delivery (includes slope protection / toe slope)	MS&D Weighted Bid Prices Item No. 156.8 and recent project costs (obtained 7/1/2024)
Site Restoration	1	LS	\$15,000	\$15,000	Site cleanup	MS&D Weighted Bid Prices Item No. 765 and recent project costs (obtained 7/1/2024)
Grout Block	740	LF	\$400	\$296,000	Restoration of existing seawall	MS&D Weighted Bid Prices Item No. 765 and recent project costs (obtained 7/1/2024)
CP Concrete	1400	CF	\$400	\$560,000	Restoration of existing seawall	MS&D Weighted Bid Prices Item No. 765 and recent project costs (obtained 7/1/2024)
Structural Fill	1400	CF	\$45	\$63,000	Restoration of existing seawall	MS&D Weighted Bid Prices Item No. 765 and recent project costs (obtained 7/1/2024)
Loam and Seed	50	SF	\$5	\$250	Loam and seed on existing slope	MS&D Weighted Bid Prices Item No. 765 and recent project costs (obtained 7/1/2024)
Contractor Mobilization/Demobilization (10%)				\$4,781,800		
Contingency (20%)				\$9,563,600		
Sub-Total:				\$46,390,000	to	\$62,208,000
Engineering and Permitting (15%)*				\$6,958,500	to	\$9,331,200
Total:				\$53,348,500	to	\$71,539,200

Alternative 2 - Composite Berms

Item	Quantity	Unit	Unit Price	Total Cost*	Notes	Source
Site Prep/Remove Control	1	LS	\$60,000	\$60,000	Fencing barriers, hubbly/hull socks, turbidity curtain	Recent project costs
Demolition and Removal	700	CF	\$175	\$122,500	Demolish existing revetment apron, and seawall as required	Recent project costs
Remove and Re-set Slope Revetment	1000	CF	\$175	\$175,000	Demolish existing stones to accommodate improvements, reinstallation	Recent project costs
Groutstone Fabric	6000	SF	\$11	\$66,000	Remove and install geotextile fabric	MS&D Weighted Bid Prices Item No. 698.1 and recent project costs (obtained 7/1/2024)
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Furnish and Install Core Stone	103500	TON	\$130	\$13,455,000	50 lb armor revetment stones with delivery	MS&D Weighted Bid Prices Item No. 156.8 and recent project costs (obtained 7/1/2024)
Furnish and Install Filter Stone	73000	TON	\$150	\$10,950,000	0.75 inch armor stone with delivery (includes slope protection / toe slope)	MS&D Weighted Bid Prices Item No. 156.8 and recent project costs (obtained 7/1/2024)
Furnish and Install Armor Stones	56000	TON	\$300	\$16,800,000	8-12 ton armor stone with delivery (includes slope protection / toe slope)	MS&D Weighted Bid Prices Item No. 156.8 and recent project costs (obtained 7/1/2024)
Site Restoration	1	LS	\$15,000	\$15,000	Site cleanup	MS&D Weighted Bid Prices Item No. 765 and recent project costs (obtained 7/1/2024)
Grout Block	740	LF	\$400	\$296,000	Restoration of existing seawall	MS&D Weighted Bid Prices Item No. 765 and recent project costs (obtained 7/1/2024)
CP Concrete	1400	CF	\$400	\$560,000	Restoration of existing seawall	MS&D Weighted Bid Prices Item No. 765 and recent project costs (obtained 7/1/2024)
Structural Fill	1400	CF	\$45	\$63,000	Restoration of existing seawall	MS&D Weighted Bid Prices Item No. 765 and recent project costs (obtained 7/1/2024)
Loam and Seed	50	SF	\$5	\$250	Loam and seed on existing slope	MS&D Weighted Bid Prices Item No. 765 and recent project costs (obtained 7/1/2024)
Contractor Mobilization/Demobilization (10%)				\$4,781,800		
Contingency (20%)				\$9,563,600		
Sub-Total:				\$46,390,000	to	\$62,208,000
Engineering and Permitting (15%)*				\$6,958,500	to	\$9,331,200
Total:				\$53,348,500	to	\$71,539,200

Alternative 3 - Composite Berms and Offshore Breakwater

Item	Quantity	Unit	Unit Price	Total Cost*	Notes	Source
Site Prep/Remove Control	1	LS	\$60,000	\$60,000	Fencing barriers, hubbly/hull socks, turbidity curtain	Recent project costs
Demolition and Removal	700	CF	\$175	\$122,500	Demolish existing revetment apron, and seawall as required	Recent project costs
Remove and Re-set Slope Revetment	1000	CF	\$175	\$175,000	Demolish existing stones to accommodate improvements, reinstallation	Recent project costs
Groutstone Fabric	6000	SF	\$11	\$66,000	Remove and install geotextile fabric	MS&D Weighted Bid Prices Item No. 698.1 and recent project costs (obtained 7/1/2024)
Furnish and Install Bedding and Crushed Stone	6900	TON	\$10	\$69,000	0.75 inch crushed stone bedding	MS&D Weighted Bid Prices Item No. 156.8 and recent project costs (obtained 7/1/2024)
Furnish and Install Core Stone	103500	TON	\$130	\$13,455,000	50 lb armor revetment stones with delivery	MS&D Weighted Bid Prices Item No. 156.8 and recent project costs (obtained 7/1/2024)
Furnish and Install Filter Stone	73000	TON	\$150	\$10,950,000	0.75 inch armor stone with delivery (includes slope protection / toe slope)	MS&D Weighted Bid Prices Item No. 156.8 and recent project costs (obtained 7/1/2024)
Furnish and Install Armor Stones	56000	TON	\$300	\$16,800,000	8-12 ton armor stone with delivery (includes slope protection / toe slope)	MS&D Weighted Bid Prices Item No. 156.8 and recent project costs (obtained 7/1/2024)
Site Restoration	1	LS	\$15,000	\$15,000	Site cleanup	MS&D Weighted Bid Prices Item No. 765 and recent project costs (obtained 7/1/2024)
Grout Block	740	LF	\$400	\$296,000	Restoration of existing seawall	MS&D Weighted Bid Prices Item No. 765 and recent project costs (obtained 7/1/2024)
CP Concrete	1400	CF	\$400	\$560,000	Restoration of existing seawall	MS&D Weighted Bid Prices Item No. 765 and recent project costs (obtained 7/1/2024)
Structural Fill	1400	CF	\$45	\$63,000	Restoration of existing seawall	MS&D Weighted Bid Prices Item No. 765 and recent project costs (obtained 7/1/2024)
Loam and Seed	50	SF	\$5	\$250	Loam and seed on existing slope	MS&D Weighted Bid Prices Item No. 765 and recent project costs (obtained 7/1/2024)
Contractor Mobilization/Demobilization (10%)				\$4,781,800		
Contingency (20%)				\$9,563,600		
Sub-Total:				\$46,390,000	to	\$62,208,000
Engineering and Permitting (15%)*				\$6,958,500	to	\$9,331,200
Total:				\$53,348,500	to	\$71,539,200

Alternative 4 - Retention Reconstruction and Berms Seawall

Item	Quantity	Unit	Unit Price	Total Cost*	Notes	Source
Site Prep/Remove Control	1	LS	\$60,000	\$60,000	Fencing barriers, hubbly/hull socks, turbidity curtain	Recent project costs
Demolition and Removal	700	CF	\$175	\$122,500	Demolish existing revetment apron, and seawall as required	Recent project costs
Remove and Re-set Slope Revetment	1000	CF	\$175	\$175,000	Demolish existing stones to accommodate improvements, reinstallation	Recent project costs
Groutstone Fabric	6000	SF	\$11	\$66,000	Remove and install geotextile fabric	MS&D Weighted Bid Prices Item No. 698.1 and recent project costs (obtained 7/1/2024)
Furnish and Install Bedding and Crushed Stone	6900	TON	\$10	\$69,000	0.75 inch crushed stone bedding	MS&D Weighted Bid Prices Item No. 156.8 and recent project costs (obtained 7/1/2024)
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Furnish and Install Armor Stones	56000	TON	\$300	\$16,800,000	8-12 ton armor stone with delivery (includes slope protection / toe slope)	MS&D Weighted Bid Prices Item No. 156.8 and recent project costs (obtained 7/1/2024)
Site Restoration	1	LS	\$15,000	\$15,000	Site cleanup	MS&D Weighted Bid Prices Item No. 765 and recent project costs (obtained 7/1/2024)
Grout Block	740	LF	\$400	\$296,000	Restoration of existing seawall	MS&D Weighted Bid Prices Item No. 765 and recent project costs (obtained 7/1/2024)
CP Concrete	1400	CF	\$400	\$560,000	Restoration of existing seawall	MS&D Weighted Bid Prices Item No. 765 and recent project costs (obtained 7/1/2024)
Structural Fill	1400	CF	\$45	\$63,000	Restoration of existing seawall	MS&D Weighted Bid Prices Item No. 765 and recent project costs (obtained 7/1/2024)
Loam and Seed	50	SF	\$5	\$250	Loam and seed on existing slope	MS&D Weighted Bid Prices Item No. 765 and recent project costs (obtained 7/1/2024)
Deep Foundation	190	LA	\$20,000	\$3,800,000	Steel H piles (piledumb and batter at 8° to L)	MS&D Weighted Bid Prices Item No. 765 and recent project costs (obtained 7/1/2024)
Contractor Mobilization/Demobilization (10%)				\$4,781,800		
Contingency (20%)				\$9,563,600		
Sub-Total:				\$46,390,000	to	\$62,208,000
Engineering and Permitting (15%)*				\$6,958,500	to	\$9,331,200
Total:				\$53,348,500	to	\$71,539,200

* This cost estimate is an estimate of probable cost for the Point Allerton Coastal Engineering Shore Protection Project. Actual cost may vary depending on when the work is completed, variable labor and material costs, and the weathering manner construction bid environment. Individual labor item cost estimates are in order of magnitude estimates with respect to the total project cost estimate.

** This cost estimate assumes that the project will be constructed as shown on the drawings, and shows the total cost for constructing each phase (top of wall elevations) of the project from existing conditions. Actual effort may vary depending on permits and the bid and construction phase sequence. The installation of a foundation was not included in cost analysis, and use of foundation is at the discretion of the contractor.

*** This cost estimate is an estimate of probable cost for the Point Allerton Coastal Engineering Shore Protection Project. Actual cost may vary depending on when the work is completed, variable labor and material costs, and the weathering manner construction bid environment. Individual labor item cost estimates are in order of magnitude estimates with respect to the total project cost estimate.

**** This cost estimate is an estimate of probable cost for the Point Allerton Coastal Engineering Shore Protection Project. Actual cost may vary depending on when the work is completed, variable labor and material costs, and the weathering manner construction bid environment. Individual labor item cost estimates are in order of magnitude estimates with respect to the total project cost estimate.

ATTACHMENT D
Edgewater Conceptual Design Analysis



Conceptual Design Analysis (Rev 01) Point Allerton, Massachusetts

October 15, 2024



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Appendix 1 - Eurotop Inputs and Outputs



INTRODUCTION

The original sea wall at Point Allerton was constructed by the US Army Corps of Engineers in 1874 as a stacked granite block structure. The granite block structure, fronted with large armor stone, has undergone numerous repairs since 1978. However, due to the increasing intensity of extreme storm events coupled with sea level rise, the structure is no longer adequate for protecting the shoreline from coastal storm damage.

Collins Engineers, Inc. (Collins) and Edgewater Resources (EWR), collectively The Team, were retained by the Massachusetts Department of Conservation and Recreation (DCR) to provide an assessment of shore protection at Point Allerton in Hull, MA. The first task of the assessment included the development of a Basis of Design (BOD) report, which provided background information on the site, a summary of the analyses and severity of the environmental factors inducing upland erosion, and recommendations for future designs to protect the upland structures.

In the BOD document, a series of explanations were presented that likely explain the failure of the structure, highlighting the original design inadequacies. The use of concrete fill at the crest of the structure, combined with its insufficient height, resulted in high overtopping volumes and high-water velocities upon reaching the crest. This led to significant erosion behind the structure, instability, settlement, and stone loss, ultimately compromising its structural integrity and protective function.

Large-scale breakwater failures most often occur behind the crest of the structure, typically a result of overtopping, as high-water volumes and velocities can erode the backslope or displace stones where armor interlock is weakest. For the Point Allerton revetment seawall, the majority of revetment failure appears to be a result of this crest overtopping. Additionally, the damage appears to be more severe in locations where expansion of the structure occurred, where tie-in locations likely became points of weaker interlock.

Following the BOD submission, The Team advanced the recommended structure repairs/modifications to the conceptual design level, including this Conceptual Design Report (CDR) which summarizes the preliminary calculations and assumptions that were described in detail in the BOD. The BOD is included as an appendix to this report, and provides detailed site information, project objectives, existing conditions, existing and projected environmental site characteristics, results of the wind and wave analysis, and the numerical modeling effort and conclusions made from this analysis.



BASIS OF DESIGN CONSIDERATIONS

The damage to the seawall at Point Allerton is mainly attributed to large overtopping volumes that reach the back of the crest. To understand how the waves approach the structure, a comprehensive numerical modeling effort was undertaken to determine the worst-case scenarios affecting the structure. A total of 18 cases were modeled, with directions ranging from the NNE to the SE. The results indicated that events coming from the ENE direction yield the highest significant wave height at the toe of the structure, resulting in the most overtopping over the crest.

Therefore, the design storm condition is based on the 0.8% (or 125-year Return Period) ENE event, combined with the design water level, which incorporates FEMA's 0.8% Still Water Elevation and is supplemented by the projected Relative Sea Level Rise according to the Representative Concentration Pathway (RCP) 8.5 scenario for the year 2070. This results in a design water level elevation of 3.66 m NAVD88 (12 ft NAVD88)¹.



Figure 1: Stillwater elevation for the design event corresponding to EL. 12 ft. NAVD88.

Due to the absence of as-built drawings from both the original construction and subsequent repairs of the seawall and revetment, certain assumptions were necessary for this analysis. The existing conditions drawings provided by Collins included approximate locations of each element, as well as cross-sections of the structure. According to these drawings, the original stacked granite wall is covered by 4–8-ton armor stones along the crest in most areas of interest (Station 4+92 to 10+53). This seawall is fronted with 8-12-

¹ Refer to the BOD document for a more detailed explanation of the design conditions.



ton armor stones placed atop core stone along the front face, with slopes varying from 1.5:1 to 2:1 (Horizontal).

Ignoring areas of damage due to settling or stone displacement, the revetment is not designed to properly absorb wave energy. The concrete fill has created impermeable and smooth surfaces that are counterproductive to energy dissipation. Insufficient crest height and crest width, combined with the existing steep revetment slopes have resulted in high overtopping velocities and volumes, causing significant erosion and structural damage landward of the revetment.

The redesign alternatives discussed in this document aim to:

- Reduce overtopping to tolerable levels.
- Increase wave energy dissipation.
- Manage storm conditions under present circumstances and future storms exacerbated by climate change.



WAVE OVERTOPPING CALCULATIONS

Overtopping of coastal structures refers to the process where wave action causes water to flow over the top of these structures, such as seawalls, breakwaters, and dikes. The extent and impact of overtopping are critical factors in coastal engineering, as they influence the stability and safety of the structures and the areas they protect. Overtopping rates are influenced by various factors, including wave height, wave period, structure geometry, and crest freeboard.

All overtopping calculations follow the formulae and methods described in the EurOtop *Manual on wave overtopping of sea defenses and related structures* (Second edition, 2018). This manual is largely based on extensive European research and is considered to be the industry standard for predicting and assessing wave overtopping seawalls, flood embankments, breakwaters and other shoreline structures.

The analysis methods described in the EurOtop Manual are primarily based upon a deterministic approach in which overtopping discharges are calculated for wave and water level conditions representing an event with a given probability or return period. The design equations require data on water levels and wave conditions at the toe of the defense structure. Input wave conditions should take account of nearshore wave transformations for which the use of numerical models is recommended. In this analysis, the nearshore wave transformations were taken into account by the SW model that simulated the transition from the offshore wave conditions to the conditions at the toe of the structure.

Understanding and predicting overtopping discharges for rubble mound structures involves detailed analysis of wave conditions, structural geometry, and material properties. This ensures that these structures provide adequate protection against coastal flooding and erosion under both current and future sea-level conditions.

Key parameters in the EurOtop formulations are defined below:

Wave height

The wave height used in the EurOtop wave run-up and overtopping formulae is the incident significant wave height H_{m0} at the toe of the structure, also called the spectral wave height.

Given that the significant wave heights at the toe vary along the Pt Allerton structure six distinct areas were identified:

1. North face area (Stations 0+00 to 2+40): Subject to relatively low wave energy.
2. Transition zone (Stations 2+40 to 3+40): Between the vertical wall and the proposed structure.
3. North face area of the proposed structure (Stations 3+40 to 4+25): Subject to moderate wave energy.
4. Northwest corner and front face of the structure (Stations 4+25 to 10+20): Subject to the highest wave energy.
5. Southeast corner of the structure (Stations 10+20 to 11+50): Transition zone between the highest wave energy and a relative low energy area.



6. South face area (Stations 11+50 to 11+81): Subject to the lowest wave energy.

These areas were identified due to the distinctly different energy losses experienced by the waves as they refract and diffract around the peninsula. The significant wave height for the design storm condition is notably higher at Station 7+00, where the waves impact directly without any change in direction (Figure 2).

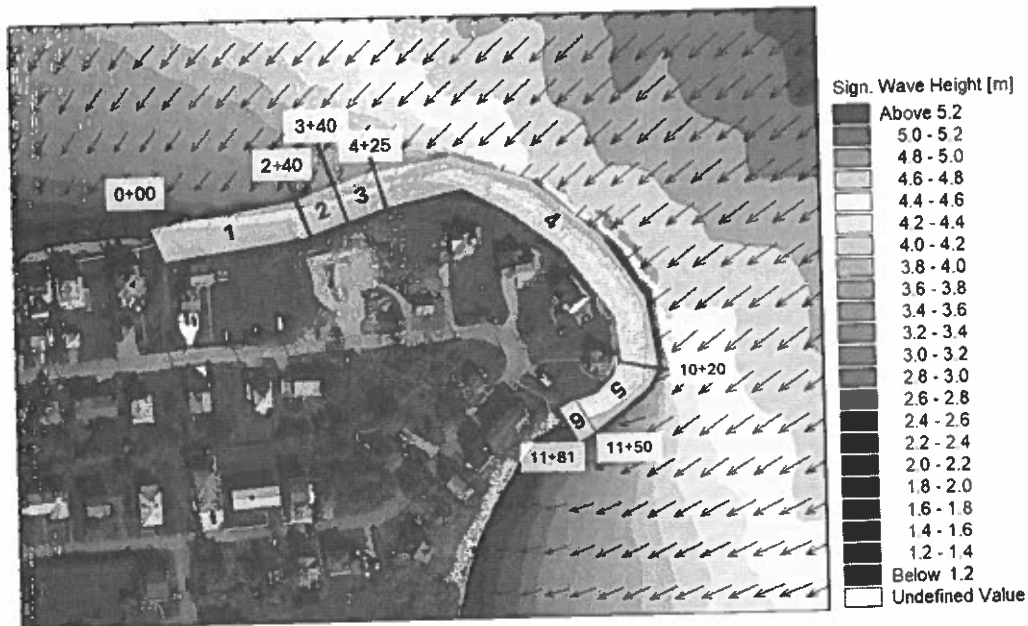


Figure 2: Significant wave height map for the design storm condition, 0.8% ENE event with a 3.66 WL.

For the purposes of preliminary design, three representative sections in the most critical areas were selected for calculations:

- Section 2+40 to 4+25
- Section 4+25 to 10+25
- Section 10+20 to 11+50

Wave conditions at the toe of the structure in these critical sections were derived from the SW model output for the design storm condition (0.8% ENE event). These wave heights are specified in Tables 2, 3, 4, and 6. Sections 0+00 to 2+40 and 11+50 to 11+81 were considered transition zones, where the new structure ties into the existing grade.

Wave steepness

Wave steepness is defined in EurOtop 2018, as the ratio of wave height to wavelength ($s_0 = H_{m0} / L_0$). This parameter indicates the wave characteristics, whether it is a typical swell sea or wind sea. Swell seas are associated with long period waves, where it is the period that becomes the main parameter that affects overtopping.



The wave steepness for the design storm condition is $s_0=0.01$ which indicates a typical swell sea.

Breaker parameter

Also called surf similarity parameter or Iribarren number is defined as $\xi_{m-1,0} = \tan\alpha/(H_{m0}/L_{m-1,0})^{1/2}$, where α is the slope of the front face of the structure and $L_{m-1,0}$ being the deep-water wavelength $gT_{m-1,0}^2/(2\pi)$.

This parameter indicates a certain type of wave breaking as shown in Figure 3.

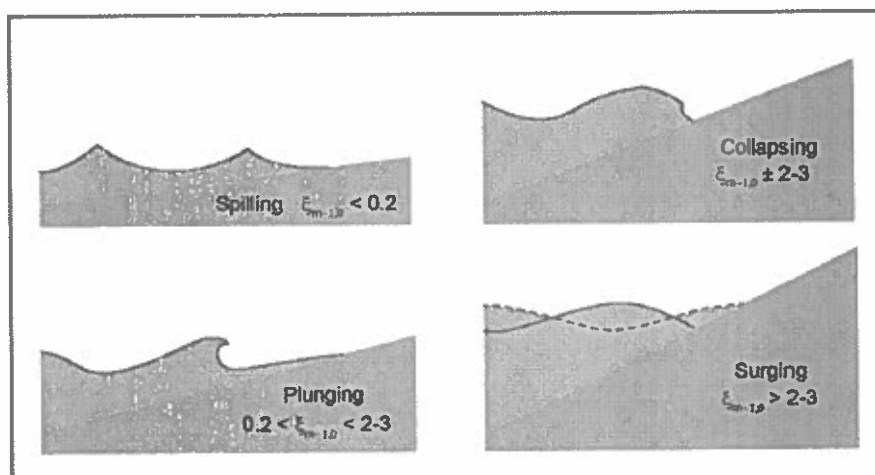


Figure 3: Breaking type on a slope. EurOtop, 2018.

The wave breaker parameter for the design storm condition is 3.27, which indicates that the waves are considering not to be breaking but surging on the structure. These occur on steep slopes where the wave does not break in the traditional sense. Instead, the wave crest remains unbroken and surges up the slope. This results in the energy dissipating by friction along the revetment surface.

Wave Runup

Wave runup is the maximum vertical extent of wave uprush on a beach or coastal structure above the still water level. It consists of two components: the wave setup and the swash. Historically, wave runup has been a critical parameter in coastal engineering and management as it determines the extent to which waves can reach and potentially impact coastal structures, beaches, and backshore areas. The 2% runup height ($R_{u2\%}$) is considered the design basis for crest level assessments. It is defined by EurOtop as the elevation exceeded by two percent of the incident waves.

However, over the past decade, the design for safety assessment has shifted towards allowable overtopping rather than wave runup.

Mean Overtopping discharge

The average overtopping discharge, q , is commonly used to assess the performance and safety of coastal structures. It represents the average volume of water overtopping per unit length of the structure per

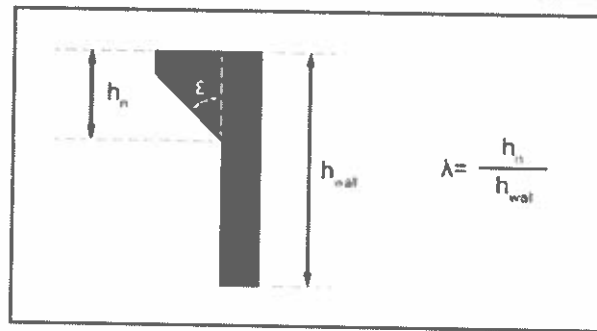
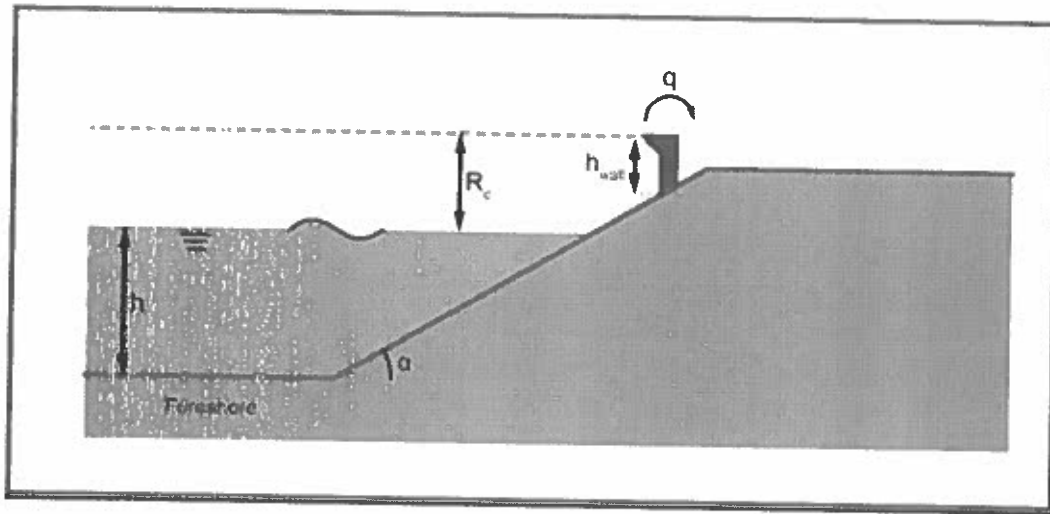


Figure 16: Configuration of a slope with a storm wall and bullnose, EurOtop, 2018.

Table 6: Preliminary dimensions for the revetment repair and wall height.

Stations	Hm0 at toe (ft)	Proposed Crest Elevation (NAVD88)	Proposed Structure Slope	Proposed Wall Elevation (NAVD88)
2+40 to 4+25	12.4	20	2:1	24
4+25 to 10+20	15.0	31	2:1	37
10+20 to 11+50	10.2	21	2:1	26